

Study of Dielectric Loaded RF Cavity



- Why a Dielectric Loaded (DL) RF cavity?
- Characterization of a dielectric loaded RF cavity
- Standard Condition – Simulation
- Standard Condition – Test Description
- Standard Condition – Data analysis and results
- Cryogenic Condition – Simulation
- Cryogenic Condition – Test Preparation
- High Power (HP) configuration study
- What's next?

Achieved during my
summer program





WHY A DIELECTRIC LOADED RF CAVITY?

MUON ACCELERATOR

OBJECTIVE: muons production, beam formation and acceleration within few milliseconds

POSSIBLE SOLUTION: helical cooling channel (=>RF structure inside a solenoid)

CONSEQUENT REQUIREMENTS FOR RF CAVITY:

- short length
- high electric field gradient (>20MV/m)
- small radial dimension
- first mode of resonance matched with external power source (Fermilab klystrons: 800 MHz)

But:

$$f \propto \frac{1}{R}$$

So:

Standard vacuum cavity DOESN'T work!



WHY A DIELECTRIC LOADED RF CAVITY? (2)

INSERTION OF DIELECTRIC MATERIAL \Rightarrow same frequency, smaller radius

PILLBOX CAVITY

$$R = \frac{2.405c}{2\pi f_{TM010} \sqrt{\epsilon_r \mu_r}}$$

$\left[\begin{array}{l} \epsilon_r: \text{relative dielectric permittivity} \\ \mu_r: \text{relative magnetic permeability} \end{array} \right]$

\rightarrow GOAL: large ϵ_r

But also \Rightarrow lower quality factor

CAVITY COMPLETELY FILLED
WITH DIELECTRIC

$$\frac{1}{Q} = \frac{P_{wall} + P_{diel}}{\omega W} = \frac{1}{Q_{wall}} + \frac{1}{Q_{diel}}$$

where:

$$Q_{diel} = \frac{\epsilon'}{\epsilon''} = \frac{1}{tg \delta}$$

$\left[\begin{array}{l} \epsilon': \text{real part of} \\ \text{dielectric constant} \\ \epsilon'': \text{imaginary part of} \\ \text{dielectric constant} \end{array} \right]$

\rightarrow GOAL: $tg \delta < 10^{-4}$



CHARACTERIZATION OF A DL RF CAVITY

Analysis of two MAIN PARAMETERS:

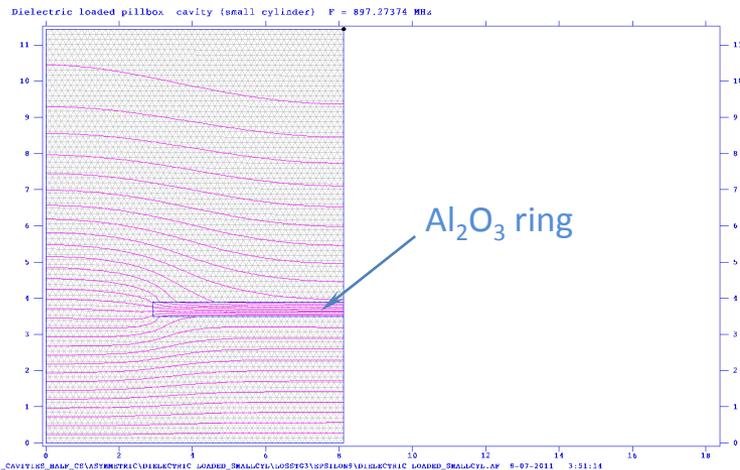
- Resonance frequency
- Quality factor

CONDITIONS considered:

- **Standard** - low power, room temperature
- **Cryogenic** - low power, cryogenic temperature (T=77K)
- **High power**

MEANS of the analysis:

SIMULATION IN SUPERFISH



→ E field direction

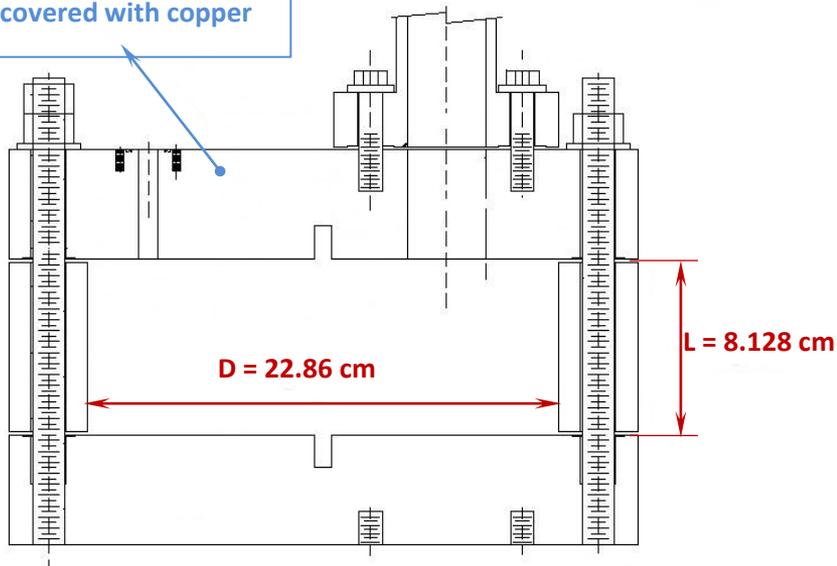
REAL TESTS



FOR REAL TESTS

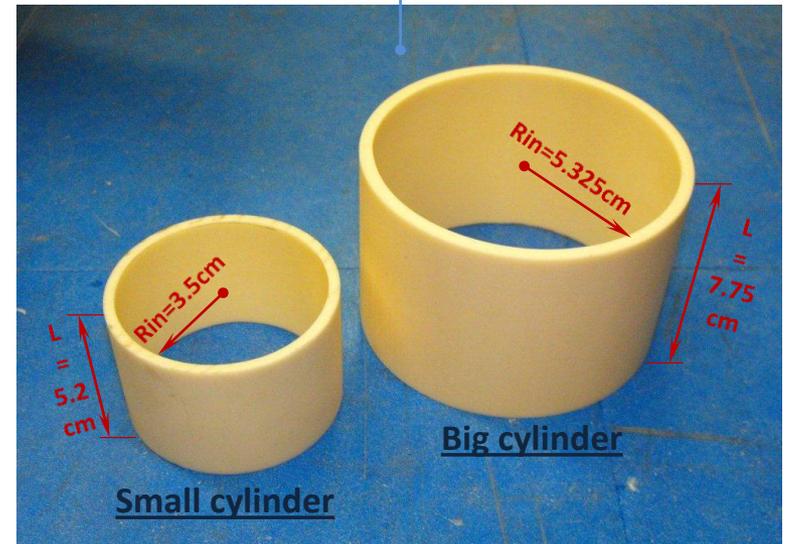
PILLBOX CAVITY

Stainless steel 316
covered with copper



DIELECTRIC RINGS

Al_2O_3 99.5%



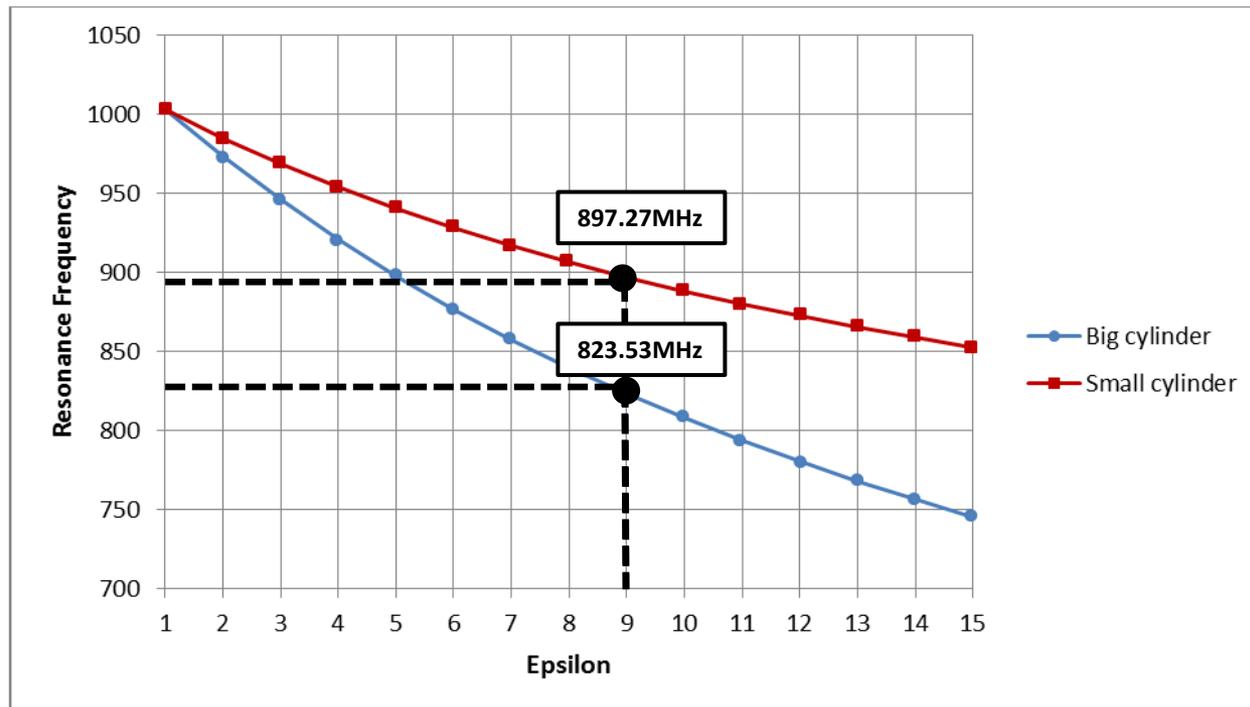


STANDARD CONDITION - SIMULATION

Empty cavity:

- $f = 1003.87$ MHz
- $Q = 22772.3$

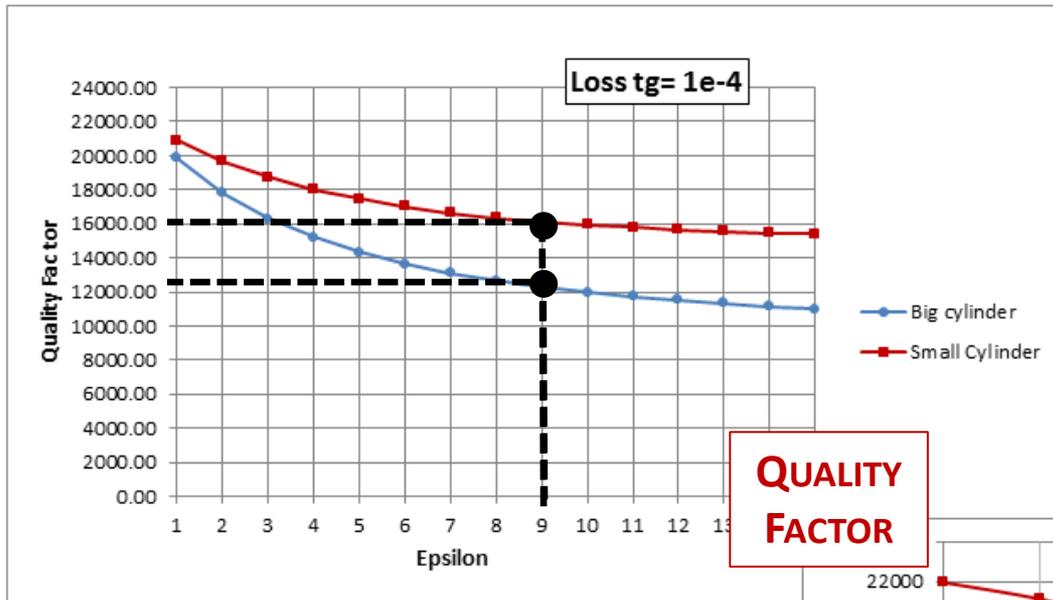
Dielectric loaded cavity:



F
R
E
Q
U
E
N
C
Y



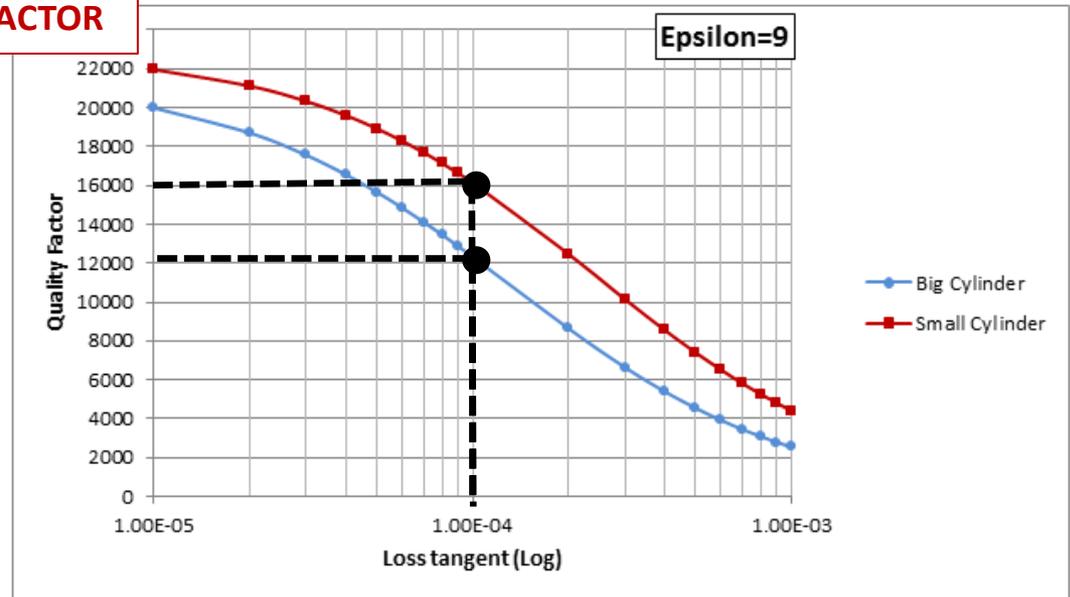
STANDARD CONDITION - SIMULATION (2)



$Q_{big} = 12310.1$

QUALITY FACTOR

$Q_{small} = 16123.6$



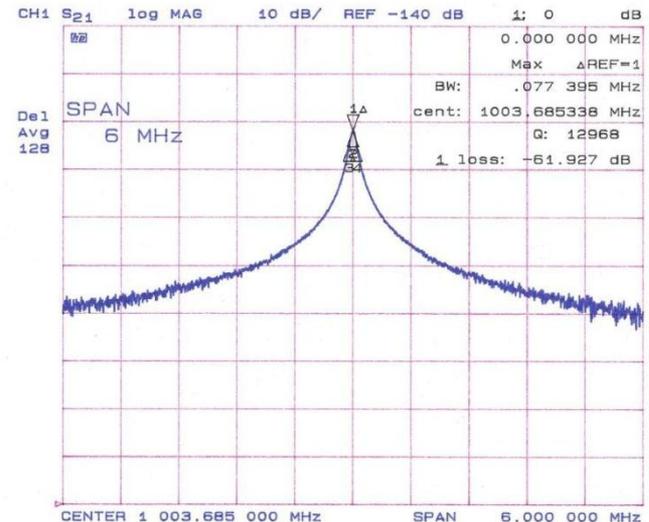


Cavity set up

- Cavity assembled through stainless steel bolts
- Systematic control of locking torque through torque meter
- Measurement through Network Analyzer (loop coupler)

Measurements for each configuration

- resonance frequency
 - good correspondence with simulation
- loaded quality factor (derivation of unloaded quality factor through coupling coefficient)
 - much lower than simulation (30-40% less)





STD CONDITION – DATA ANALYSIS AND RESULTS

Model used to analyze the data:

- lower Q = higher wall resistivity

→ estimate an equivalent resistivity for the cavity

$$\Omega = 4.677E-6 \text{ Ohm/cm } (\pm 4\%)$$

- Introduce this value in the model for the dielectric loaded cavity

→ extract dielectric properties of the ceramic rings

Final results:

SMALL CYLINDER

$$f = 897.96 (\pm 0.97) \text{ MHz}$$
$$Q = 11823.1 (\pm 1037.1)$$



$$\epsilon = 8.925 (\pm 0.125)$$
$$\text{tg}\delta = 7.28E-5 (\pm 4.92E-5)$$

BIG CYLINDER

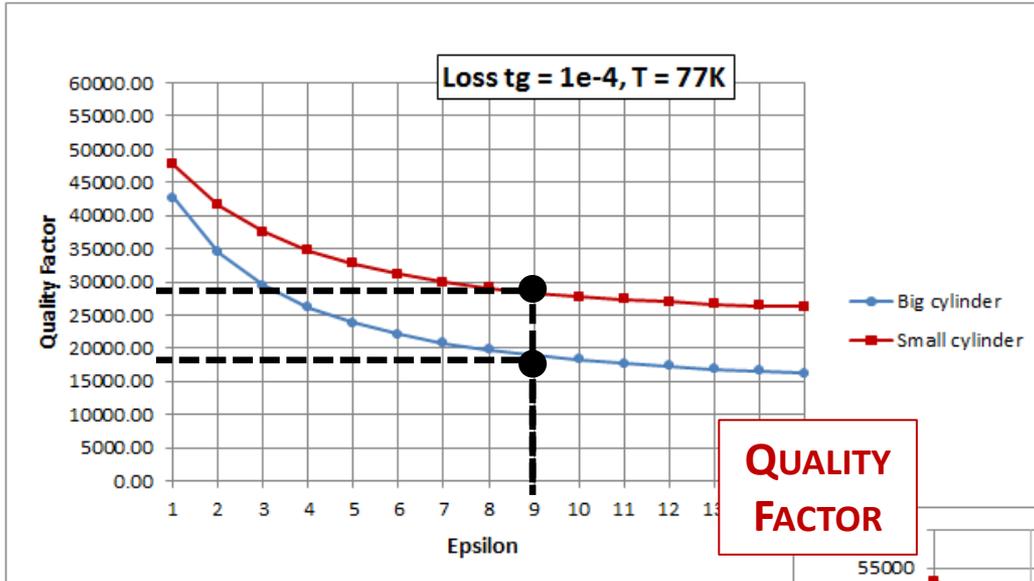
$$f = 814.30 (\pm 0.81) \text{ MHz}$$
$$Q = 9415.89 (\pm 828.6)$$



$$\epsilon = 9.595 (\pm 0.134)$$
$$\text{tg}\delta = 8.17E-5 (\pm 5.52E-5)$$



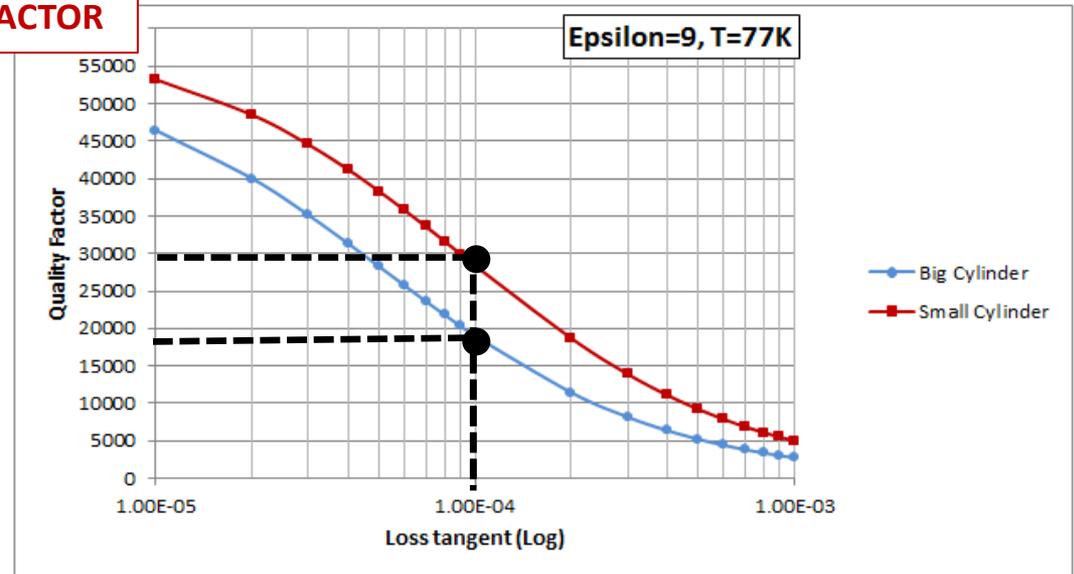
CRYOGENIC CONDITION – SIMULATION

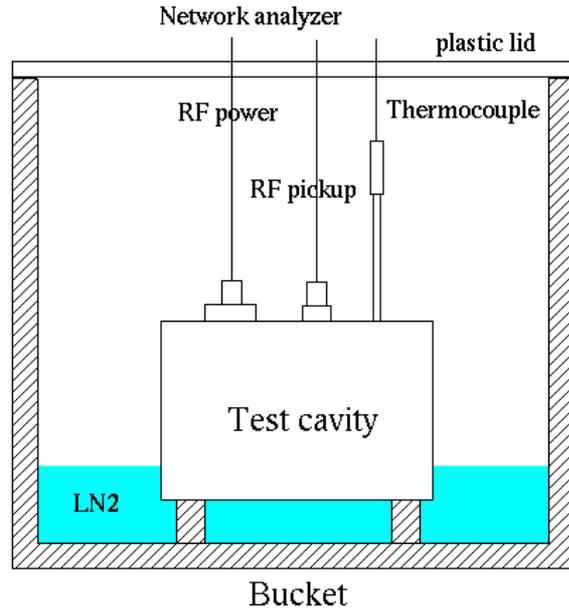


$$Q_{big} = 18966.9$$

QUALITY FACTOR

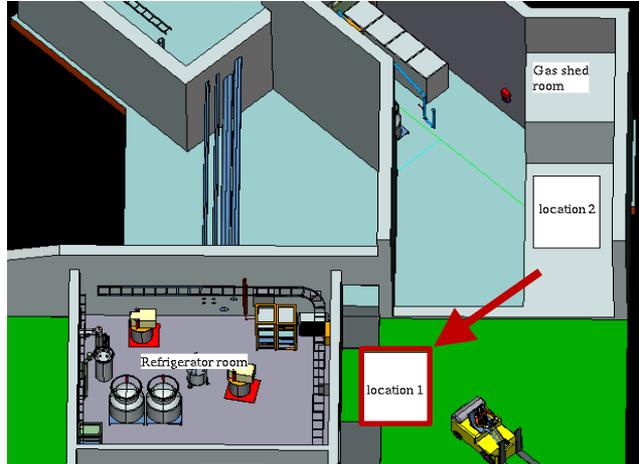
$$Q_{small} = 28361.7$$





System set up:

- proper bucket to contain the LN2
- temperature sensor
- feeding probe for He



Location choice

- ODH requirements
- need for power supply

TEST

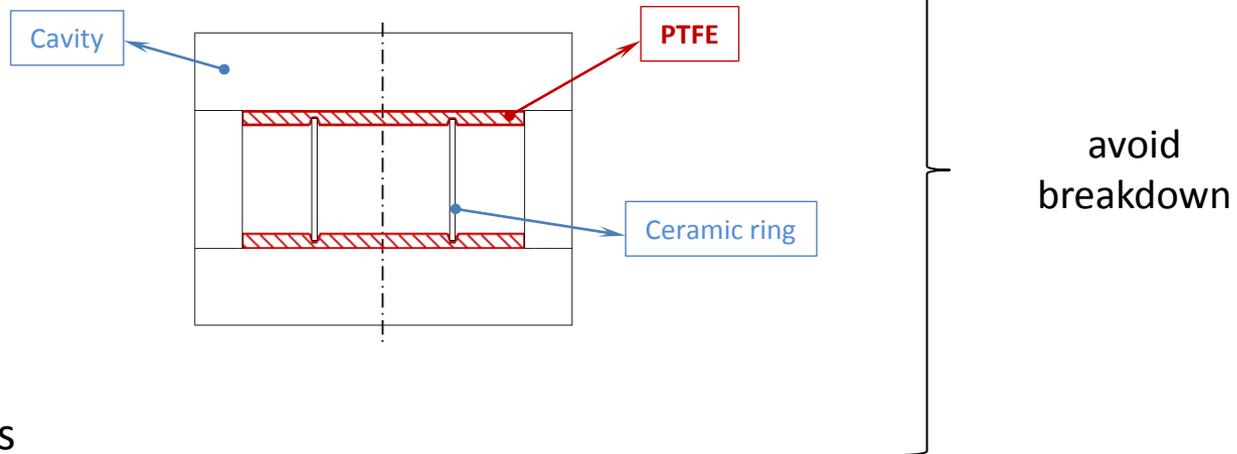


First result:

$$Q_{\text{empty}} = 23774.2$$

Future High Power Tests

- Location: MTA
- Only big cylinder (for the smaller one the frequency shift is too small)
- Teflon holder for the ceramic ring



- Cavity filled with gas

➔ **GOAL: study the feasibility of using a gas filled dielectric loaded RF cavity at HP**



CONCLUSIONS

ACHIEVEMENTS:

LOW POWER ANALYSIS

- Description of the behavior of a dielectric loaded RF cavity under different conditions through simulation
- *At room temperature:*
 - Realization of a complete set of test for the empty cavity
 - Analysis of the data and extraction of the dielectric properties of the ceramic
 - quite good agreement with expected value, provided by the company, both for ϵ_r (exp. ≈ 9) and loss tangent (exp. $\approx 10^{-4}$)
 - ERROR: mainly due to the sensitivity of the measurements to variation in real resistivity of the cavity
- *At cryogenic temperature:*
 - Set up of the equipment and definition of the procedure to follow for the test
 - Realization of test for the empty cavity

HIGH POWER ANALYSIS

- Design of Teflon holder for the ceramic ring to use during HP test

WHAT'S NEXT?

- Complete cryogenic tests and analyze the data to extract how the dielectric properties of the ceramic ring change with temperature and how this affects the behavior of the cavity
- Complete the set up of HP configuration and run the test

If all the GOALS of the study will be achieved

- Dielectric material:
 - $\epsilon_r > 9$, $\text{tg}\delta < 10^{-4}$
- Electric gradient $> 20\text{MV/m}$

We'll prove the feasibility of a HPDL RF cavity

such a cavity could allow the realization of a helical cooling channel
AND
it could be applied also to other type of muon cooling channel

GOOD RESOURCE FOR MUON COLLIDER REALIZATION